APPENDIX A – FACILITIES EVALUATED BY REID MIDDLETON

Building and Other Structures

- August Pump Station and Gatehouse
- Boulevard Park Well and Chlorination Building
- Broadway Pump Station and Chlorination Building
- Burien Pump Station
- First Hill Pump Station
- Highland Park Pump Station
- Lake Youngs Pump Station (new)
- Lake Youngs Treatment Plant
 - Operations Building
 - Lake Youngs Intake and Raw Water Pump Station
 - o Lake Youngs Ozone Generation and Injection Building
 - o UV and Chemical Building
- Landsburg Tunnel Gatehouse
- Maple Leaf P.S. and Gatehouse
- Operations and Control Center
 - Administration Building (OCC)
 - Warehouse (OCC)
 - Flammable Liquid Storage (OCC)
 - Pipe Carpentry Shop (OCC)
 - Vehicle Maintenance Bldg (OCC)
 - Meter Shop (OCC)
- Riverton Well and Chlorination Building
- Tolt Filtration Plant:
 - o Administration Building
 - Filter Gallery
 - Ozone Room/Contact Tank
- Warren Avenue Pump Station
- West Seattle Pump Station

Concrete and Earthen Reservoirs

- Eastside
- Lake Forest Park
- Lake Youngs Clearwells (North and South)
- Lincoln Reservoir
- Magnolia Reservoir
- Riverton Heights
- Soos North
- Soos South
- Tolt Clearwell
- View Ridge

Ground-Supported and Elevated Steel Tanks

- Charleston Standpipe
- Control Works Tanks (North and South)
- Foy Standpipe
- Richmond Highland #2 Elevated Tank
- Trenton Tanks (North and South)
- Trenton Tank South

APPENDIX B – HYDRAULIC MODELING RESULTS

M7.0 Seattle Fault Zone Base Case (No Improvements) Hydraulic Modeling Results



Seattle Fault Seismic Event

Base No system modifications

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	250,512	230,344	20,168	71%	232.1
3	228,115	211,496	16,619	62%	186.3
12	178,256	164,131	14,126	45%	77.7
16	54,565	50,885	3,680	7%	40.8
22	24,329	23,595	734	4%	15.4
32	21,286	21,286	-	3%	3.7
48	-	-	-	2%	0.5

Model Regions Forced Out of Service During Simulation

S1

S2

S3

S4

Time Region

3

15

21

32

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

2. System Positive Pressure based on number of junctions above 0 psi

3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm

4. Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

del Results Figur	re Index			
Fig. 1 Hr O	Fig. 5 Hr 8	Fig. 9 Hr 16	Fig. 13 Hr 24	Fig. 17 Hr 40
Fig. 2 Hr 2	Fig. 6 Hr 10	Fig. 10 Hr 18	Fig. 14 Hr 28	Fig. 18 Hr 44
Fig. 3 Hr 4	Fig. 7 Hr 12	Fig. 11 Hr 20	Fig. 15 Hr 32	Fig. 19 Hr 48
Fig. 4 Hr 6	Fig. 8 Hr 14	Fig. 12 Hr 22	Fig. 16 Hr 36	



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M9.0 Cascadia Subduction Zone Base Case (No Improvements) Hydraulic Modeling Results



Cascadia Seismic Event

Base No system modifications

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Satisfied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	236,361	214,034	22,326	77%	270.8
3	228,503	206,337	22,166	76%	228.4
12	182,743	164,714	18,029	60%	118.7
17	106,508	94,253	12,255	31%	61.1
22	20,590	20,590	-	2%	39.5
32	-	-	-	2%	38.6
48	-	-	-	2%	38.6

Model Regions Forced Out of Service During Simulation

Service During Simul			
Time	Region		
16	C1		
17	C3		
20	C2		

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

- 2. System Positive Pressure based on number of junctions above 0 psi
- 3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 1	Hr O	Fig. 5	H r 8	Fig. 9	Hr 16
Fig. 2	Hr 2	Fig. 6	Hr 10	Fig. 10	Hr 18
Fig. 3	Hr 4	Fig. 7	Hr 12	Fig. 11	Hr 20
Fig. 4	Hr 6	Fig. 8	H r 14	Fig. 12	Hr 22

Fig. 13 Hr 24



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M7.0 Seattle Fault Zone Case 1 (20 Year Improvements) Hydraulic Modeling Results



1/26/2018

Seattle Fault Seismic Event

 $\textbf{Case 1} \hspace{0.1 cm} \textbf{Isolation and Control and Most-Critical Facility Upgrades}$

Some facilities shown below are now functional Assume that certain emitters are now zero and that certain areas are automatically isolated to prevent leakage

In Service Storage Eastside Reservoir Magnolia Bluff Elevated Tank Magnolia Reservoir Riverton Heights Reservoir

In Service Facilities
Lincoln PS
Broadway PS
Spokane Street PS
West Seattle PS

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	139,011	112,189	26,823	80%	287.2
3	125,861	99,889	25, 9 72	78%	264.3
12	114,374	89,685	24,689	73%	201.1
22	39,026	31,588	7,437	15%	140.0
32	38,730	31,292	7,437	15%	108.0
48	14,716	10,501	4,215	11%	66.8

Model Regions Forced Out of Service During Simulation

Time	Region
1	S10
16	S6
22	S2
45	S8
47	S4

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

2. System Positive Pressure based on number of junctions above 0 psi

3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm

 Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 1.1 Hr 0	Fig. 1.5 Hr 8	Fig. 1.9 Hr 16	Fig. 1.13 Hr 24	Fig. 1.17 Hr 40
Fig. 1.2 Hr 2	Fig. 1.6 Hr 10	Fig. 1.10 Hr 18	Fig. 1.14 Hr 28	Fig. 1.18 Hr 44
Fig. 1.3 Hr 4	Fig. 1.7 Hr 12	Fig. 1.11 Hr 20	Fig. 1.15 Hr 32	Fig. 1.19 Hr 48



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M7.0 Seattle Fault Zone Case 2 (50 Year Improvements) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 2 Isolation and Control and All Critical Facility Upgrades

Cedar River Pipeline #2 Functional and West Seattle Pipeline Functional

Assume that certain emitters are now zero and

that certain areas are automatically isolated to

prevent leakage

All facilities shown below are now functional

In Service Storage
Eastside Reservoir
Magnolia Bluff Elevated Tank
Magnolia Reservoir
Riverton Heights Reservoir
Beverly Park Elevated Tank
Charlestown Standpipe
Foy Standpipe
View Ridge Reservoir
Volunteer Park Standpipe

In Service Facilities
Lincoln PS
Broadway PS
Spokane Street PS
West Seattle PS
Trenton PS
Augusta PS
Fairwood PS

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	166,493	135,655	30,838	90%	294.3
3	153,225	122,708	30,517	90%	273.6
12	139,924	109,922	30,002	86%	219.7
22	133,403	104,028	29,375	83%	162.6
32	89,645	69,424	20,222	56%	119.8
48	50,748	34,795	15,954	48%	87.0

Model Regions Forced Out of

Service During Simulation

Time	Region
22	S7
24	S11
27	S6
47	S4
47	S 8

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

2. System Positive Pressure based on number of junctions above 0 psi

3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm

 Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 2.1	Hr 0 Fig. 2.5	Hr 8 Fig. 2	2.9 Hr 16 Fi	ig. 2.13 Hr 24	Fig. 2.17 Hr 40
Fig. 2.2	Hr 2 Fig. 2.6	Hr 10 [;] ig. 2.	10 Hr 18 🛛 Fi	ig. 2.14 Hr 28	Fig. 2.18 Hr 44
Fig. 2.3	Hr 4 Fig. 2.7	Hr 12 [;] ig. 2.	11 Hr 20 🛛 Fi	ig. 2.15 Hr 32	Fig. 2.19 Hr 48
Fig. 2.4	Hr 6 Fig. 2.8	Hr 14 [;] ig. 2.	12 Hr 22 Fi	ig. 2.16 Hr 36	



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M7.0 Seattle Fault Zone Case 3 (20 Year Improvements Plus Roosevelt and Volunteer Park Reservoirs Online) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 3 Same as Case 1

Roosevelt and Volunteer Park Reservoir are Functional

In Service Storage
Eastside Reservoir
Magnolia Bluff Elevated Tank
Magnolia Reservoir
Riverton Heights Reservoir
Roosevelt Reservoir
Volunteer Park Reservoir

In Service Facilities Lincoln PS Broadway PS Spokane Street PS West Seattle PS

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	149,899	121,992	27,907	90%	340.7
3	149,243	121,992	27,251	90%	316.0
12	128,219	101,479	26,740	86%	248.1
22	91,632	72,635	18,997	66%	181.3
32	59,312	45,916	13,397	45%	125.0
48	18,994	12,378	6,616	17%	80.1

Model Regions Forced Out of Service During Simulation

Time	Region
1	S10
16	S6
31	S2
38	58

Model Simulation Notes

- 1. Satisfied Demands assume junction pressure greater than 0 psi
- 2. System Positive Pressure based on number of junctions above 0 psi
- 3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 3.1	Hr O	Fig. 3.5	Hr 8
Fig. 3.2	Hr 2	Fig. 3.6	Hr 10
Fig. 3.3	H r 4	Fig. 3.7	Hr 12
Fig. 3.4	Hr 6	Fig. 3.8	H r 14

Fig. 3.9	Hr 16	Fig. 3.13	Hr 24	Fig. 3.17	Hr 40
Fig. 3.10	Hr 18	Fig. 3.14	Hr 28	Fig. 3.18	Hr 44
Fig. 3.11	Hr 20	Fig. 3.15	Hr 32	Fig. 3.19	Hr 48
Fig. 3.12	Hr 22	Fig. 3.16	Hr 36		



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M7.0 Seattle Fault Zone Case 4 (50 Year Improvements Plus Roosevelt and Volunteer Park Reservoirs Online) Hydraulic Modeling Results



2/2/2018

Seattle Fault Seismic Event

Case 4 Same as Case 2 Roosevelt and Volunteer Park Reservoir are Functional

- In Service Storage Eastside Reservoir Magnolia Bluff Elevated Tank Magnolia Reservoir Riverton Heights Reservoir Beverly Park Elevated Tank Charlestown Standpipe Foy Standpipe View Ridge Reservoir Volunteer Park Standpipe Roosevelt Reservoir Volunteer Park Reservoir
- In Service Facilities Lincoln PS Broadway PS Spokane Street PS West Seattle PS Trenton PS Augusta PS Fairwood PS

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	172,157	141,232	30,926	92%	347.8
3	159,710	128,809	30,901	91%	325.8
12	150,350	11 9 ,736	30,614	89%	266.9
22	138,135	108,736	29,399	86%	205.1
32	129,636	102,448	27,187	82%	149.7
48	68,790	48,462	20,328	62%	91.5

Model Regions Forced Out of Service Durina Simulation

Service During Simula			
Time	Region		
13	S7		
24	S11		
27	S6		
47	S4		
47	S8		

Fig. 4.1 Hr 0 Fig. 4.2 Hr 2 Fig. 4.3 Hr 4 Fig. 4.4 Hr 6

Model Simulation Notes

- 1. Satisfied Demands assume junction pressure greater than 0 psi
- 2. System Positive Pressure based on number of junctions above 0 psi
- 3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 4.5 H	r 8 Fig. 4	.9 Hr 16	Fig. 4.13	H r 2 4	Fig. 4.17	Hr 40
Fig. 4.6 H	r 10 Fig. 4.1	0 Hr 18	Fig. 4.14	Hr 28	Fig. 4.18	Hr 44
Fig. 4.7 H	r 12 Fig. 4.	11 Hr 20	Fig. 4.15	Hr 32	Fig. 4.19	H r 48
Fig. 4.8 H	r 14 Fig. 4.1	2 Hr 22	Fig. 4.16	Hr 36		



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M7.0 Seattle Fault Zone Case 5 (No Improvements Except Cedar Transmission System is Assumed to be Functional) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 5 Same as "Base" case CRPL #1, #2, #3 are Functional

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	329,851	303,593	26,259	92%	251.1
3	326,218	289,682	36,535	82%	210.5
12	261,364	240,666	20,698	69%	123.9
22	218,461	200,709	17,752	66%	56.9
32	214,803	197,800	17,003	64%	26.1
48	180,543	164,584	15, 9 58	60%	16.5

Model Regions Forced Out of

\$5

Service During SimulationTimeRegion3\$132\$4

35

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

2. System Positive Pressure based on number of junctions above 0 psi

3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm

 Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 5.1	Hr 0 Fig. 5.5	Hr 8	Fig. 5.9 Hr :	16 Fig. 5.13	Hr 24 F	[:] ig. 5.17	Hr 40
Fig. 5.2	Hr 2 Fig. 5.6	Hr 10 I	Fig. 5.10 Hr :	18 Fig. 5.14	Hr 28 F	ig. 5.18 [:]	H r 44
Fig. 5.3	Hr 4 Fig. 5.7	Hr 12 I	Fig. 5.11 Hr :	20 Fig. 5.15	Hr 32 F	ig. 5.19	Hr 48
Fig. 5.4	Hr 6 Fig. 5.8	Hr 14 I	Fig. 5.12 Hr 3	22 Fig. 5.16	Hr 36	-	



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M7.0 Seattle Fault Zone Case 6 (No Improvements Except Cedar Transmission System is Assumed to be Functional and Damage Isolation Systems Have Been Installed) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 6 Same as Case 5

Assume that certain emitters are now zero and that certain areas are automatically isolated to prevent leakage

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	145,539	121,380	24,159	88%	232.1
3	142,811	118,735	24,076	88%	217.3
12	126,254	107,476	18,778	75%	182.6
22	120,986	102,368	18,618	73%	149.1
32	120,437	101,820	18,618	73%	119.2
48	100,569	82,773	17,796	70%	85.2

Model Regions Forced Out of

Service During Simulation						
Time	Region					
6	S1					
38	\$8					

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

- 2. System Positive Pressure based on number of junctions above 0 psi
- 3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 6.1	Hr O	Fig. 6.5	H r 8	Fig. 6.9	Hr 16	Fig. 6.13	Hr 24	Fig. 6.17	Hr 40
Fig. 6.2	Hr 2	Fig. 6.6	Hr 10	Fig. 6.10	H r 18	Fig. 6.14	Hr 28	Fig. 6.18	H r 44
Fig. 6.3	H r 4	Fig. 6.7	Hr 12	Fig. 6.11	Hr 20	Fig. 6.15	Hr 32	Fig. 6.19	Hr 48
Fig. 6.4	Hr 6	Fig. 6.8	Hr 14	Fig. 6.12	Hr 22	Fig. 6.16	Hr 36		



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M7.0 Seattle Fault Zone Case 7 (No Improvements Except Tolt Transmission System is Assumed to be Functional) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 7 Same as "Base" case **Tolt Pipelines are Functional**

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	250,512	230,344	20,168	71%	232.1
3	228,068	211,560	16,508	60%	188.7
12	178,531	164,405	14,126	45%	87.1
22	53,577	49,897	3,680	7%	34.4
32	50,317	47,371	2,946	5%	4.1
48	39,050	36,105	2,946	5%	1.0

Model Regions Forced Out of Service During Simulation

Time Region 3 S1 15 S2 32 **\$**4 34 S3

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

2. System Positive Pressure based on number of junctions above 0 psi

3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm

4. Reported Demands & Positive Pressure ignores transmission mains

East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

odel Results Figure index									
Fig. 7.1 Hr 0	Fig. 7.5	Hr 8	Fig. 7.9	Hr 16	Fig. 7.13	Hr 24	Fig. 7.17	Hr 40	
Fig. 7.2 Hr 2	Fig. 7.6	Hr 10	Fig. 7.10	Hr 18	Fig. 7.14	Hr 28	Fig. 7.18	H r 44	
Fig. 7.3 Hr 4	Fig. 7.7	Hr 12	Fig. 7.11	Hr 20	Fig. 7.15	Hr 32	Fig. 7.19	Hr 48	
Fig. 7.4 Hr 6	Fig. 7.8	Hr 14	Fig. 7.12	Hr 22	Fig. 7.16	Hr 36			



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M7.0 Seattle Fault Zone Case 8 (No Improvements But Roosevelt and Volunteer Park Reservoirs Online) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 8 Same as "Base" case

Roosevelt and Volunteer Park Reservoir are Functional

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	271,913	249,543	22,370	78%	285.5
3	252,683	233,750	18,933	68%	236.2
12	186,861	171,987	14,874	50%	117.5
22	41,910	35,431	6,480	22%	32.3
32	10,741	10,741	-	3%	4.0
48	-	-	-	2%	0.5

Model Regions Forced Out of

Service During Simulation

	5
Time	Region
3	S1
20	S2
32	S4
35	S3

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

2. System Positive Pressure based on number of junctions above 0 psi

3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm

 Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 8.1 Hr 0

Fig. 8.2 Hr 2 Fig. 8.3 Hr 4

Fig. 8.4 Hr 6

re Index							
Fig. 8.	5 Hr 8	Fig. 8.9	Hr 16	Fig. 8.13	Hr 24	Fig. 8.17	Hr 40
Fig. 8.	6 Hr 10	Fig. 8.10	Hr 18	Fig. 8.14	Hr 28	Fig. 8.18	H r 44
Fig. 8.	7 Hr 12	Fig. 8.11	Hr 20	Fig. 8.15	Hr 32	Fig. 8.19	Hr 48
Fig. 8.	8 Hr 14	Fig. 8.12	Hr 22	Fig. 8.16	Hr 36		



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M7.0 Seattle Fault Zone Case 9 (No Improvements Except Tolt Transmission System is Assumed to be Functional and Damage Isolation Systems Have Been Installed) Hydraulic Modeling Results



Seattle Fault Seismic Event

Case 9 Same as Case 7

Assume that certain emitters are now zero and that certain areas are automatically isolated to prevent leakage

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	111,997	89,802	22,195	81%	232.1
3	109,109	87,065	22,044	79%	213.2
12	90,857	74,412	16,445	65%	166.2
22	83,462	67,902	15,560	60%	119.1
32	41,434	35,937	5,498	25%	95.0
48	41,137	35,639	5,498	24%	61.6

Model Regions Forced Out of

Service During Simulation						
Time	Region					
6	S1					
23	\$2					

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

- 2. System Positive Pressure based on number of junctions above 0 psi
- 3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

Fig. 9.1	Hr O Fig. 1	9.5 Hr 8	Fig. 9.9 Hr 16	Fig. 9.13	H r 2 4	Fig. 9.17	Hr 40
Fig. 9.2	Hr 2 Fig.	9.6 Hr 10	Fig. 9.10 Hr 18	Fig. 9.14	Hr 28	Fig. 9.18	H r 44
Fig. 9.3	Hr 4 Fig. 1	9.7 Hr 12	Fig. 9.11 Hr 20	Fig. 9.15	Hr 32	Fig. 9.19	Hr 48
Fig. 9.4	Hr6 Fig.	9.8 Hr 14	Fig. 9.12 Hr 22	Fig. 9.16	Hr 36		



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M7.0 Seattle Fault Zone Case 10 (20 Year Improvements Plus One of the Cedar River Pipelines is Functional) Hydraulic Modeling Results



Water Distribution System Seismic Modeling 2/6/2018

Seattle Fault Seismic Event

Case 10 Same as Case 1

CRPL #2 and West Seattle Pipelines are Functional

In Service Storage
Eastside Reservoir
Magnolia Bluff Elevated Tank
Magnolia Reservoir
Riverton Heights Reservoir

In Service Facilities
Lincoln PS
Broadway PS
Spokane Street PS
West Seattle PS

Model Results

Time (hrs)	Total System Demand (gpm)	Emiter Flows (gpm)	Supplied Demands (gpm)	System Positive Pressure (%)	Available System Storage (MG)
0	149,870	121,579	28,291	87%	287.2
3	136,871	109,236	27,635	86%	268.3
12	123,522	96,801	26,721	82%	219.6
22	123,458	96,990	26,468	80%	166.3
32	82,052	63,604	18,447	52%	125.4
48	45,414	31,322	14,092	44%	90.7

Model Regions Forced Out of

Service During Simulatio					
Time	Region				
1	S10				
29	S6				
45	S4				
45	S8				

Model Simulation Notes

1. Satisfied Demands assume junction pressure greater than 0 psi

- 2. System Positive Pressure based on number of junctions above 0 psi
- 3. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- Reported Demands & Positive Pressure ignores transmission mains East of Lake Forest Park Reservoir (Total Demand = 13,786 gpm)

Model Results Figure Index

del Results Figure muex									
Fig. 10.1	Hr O	Fig. 10.5	Hr 8	Fig. 10.9	Hr 16	Fig. 10.13	Hr 24	Fig. 10.17	Hr 40
Fig. 10.2	Hr 2	Fig. 10.6	Hr 10	Fig. 10.10	Hr 18	Fig. 10.14	Hr 28	Fig. 10.18	Hr 44
Fig. 10.3	Hr 4	Fig. 10.7	Hr 12	Fig. 10.11	Hr 20	Fig. 10.15	Hr 32	Fig. 10.19	Hr 48
Fig. 10.4	Hr6	Fig. 10.8	Hr 14	Fig. 10.12	Hr 22	Fig. 10.16	Hr 36		



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M7.0 Seattle Fault Zone Transmission Pipeline Base Case (No Improvements) Hydraulic **Modeling Results**



Seattle Fault Seismic Event **Transmission Pipeline Simulations**

Base 2018	Water from Tolt Filtration Plant cannot be conveyed west					
	Water from Control Works (Cedar System) cannot be conveyed into the					
	distibution system					
	Other assumptions are the same as the Base SFZ scenario					

Model Results

		Emitter				
Time Total System		Flows	Supplied Demands	System Positive	Available System	
(hrs)	Demand (gpm)	(gpm)	(gpm)	Pressure (%)	Storage (MG)	
0	257,089	226,005	31,084	64%	244.3	
3	239,604	214,223	25,381	57%	196.5	
12	184,673	162,975	21,697	42%	85.1	
22	31,108	23,889	7,219	6%	29.5	
32	28,321	21,837	6,485	5%	14.4	
48	6,485	0	6,485	5%	11.5	

Model Regions Forced Out of Service During Simulation

Service During Simula						
Time	Region					
3	S1					
15	S2					
21	S3					
21	S8					
32	S4					

Model Simulation Notes

- 1. All wholesale customers assumed to start with 1.8 multiplier (max day demands)
- 2. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- 3. Total Model Demands with elevated wholesale customers is 91,957 gpm
- 4. Satisfied Demands assume junction pressure greater than 0 psi
- 5. System Positive Pressure based on number of junctions above 0 psi out of the entire model

Model Results Figure Index

woder nesures righte maex									
Fig. 11.1	Hr O	Fig. 11.5	Hr 8	Fig. 11.9	Hr 16	Fig. 11.13	Hr 24	Fig. 11.17	Hr 40
Fig. 11.2	Hr 2	Fig. 11.6	H r 10	Fig. 11.10	H r 18	Fig. 11.14	Hr 28	Fig. 11.18	Hr 44
Fig. 11.3	H r 4	Fig. 11.7	Hr 12	Fig. 11.11	Hr 20	Fig. 11.15	Hr 32	Fig. 11.19	Hr 48
Fig. 11.4	Hr 6	Fig. 11.8	H r 14	Fig. 11.12	Hr 22	Fig. 11.16	Hr 36		





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M7.0 Seattle Fault Zone Transmission Pipeline Year 2045 Improvement Case Hydraulic Modeling Results



4/4/2018

Seattle Fault Seismic Event Transmission Pipeline Simulations

Case 2045 A Water from Tolt Filtration Plant cannot be conveyed west; Eastside Supply Line is open; Tolt Eastside Pipes 7623, 7113, 7079, 7509 are closed; Facility upgrades are the same as distribution system Case 1; Water from Control Works (Cedar System) cannot be conveyed into the distibution system.

Model Results

		Emitter				
Time	Total System	Flows	Supplied Demands	System Positive	Available System	
(hrs)	Demand (gpm)	(gpm)	(gpm)	Pressure (%)	Storage (MG)	
0	337,537	279,583	57,953	75%	299.5	
3	301,701	247,840	53,862	73%	242.3	
12	219,606	177,790	41,815	49%	107.2	
22	68,141	41,920	26,221	11%	41.0	
32	54,703	31,501	23,202	9%	14.2	
48	24,771	17,638	7,133	6%	11.6	

Model Regions Forced Out of

Service During Simulation						
Time	Region					
9	S6					
15	S1					
15	S2					
26	S4					
26	S3					
26	S8					
33	T1					

Model Simulation Notes

- 1. All wholesale customers assumed to start with 1.8 multiplier (max day demands)
- 2. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- 3. Total Model Demands with elevated wholesale customers is 91,957 gpm
- 4. Satisfied Demands assume junction pressure greater than 0 psi
- System Positive Pressure based on number of junctions above 0 psi out of the entire model

Model Results Figure Index

Fig. 12.1	H r 0	Fig. 12.5	Hr8	Fig. 12.9	Hr 16	Fig. 12.13	H r 2 4	Fig. 12.17	Hr 40
Fig. 12.2	Hr 2	Fig. 12.6	Hr 10	Fig. 12.10	Hr 18	Fig. 12.14	Hr 28	Fig. 12.18	H r 44
Fig. 12.3	H r 4	Fig. 12.7	Hr 12	Fig. 12.11	Hr 20	Fig. 12.15	Hr 32	Fig. 12.19	H r 48
Fig. 12.4	Hr 6	Fig. 12.8	Hr 14	Fig. 12.12	Hr 22	Fig. 12.16	Hr 36		





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M7.0 Seattle Fault Zone Transmission Pipeline Year 2045 Improvement Case with Roosevelt and Volunteer Reservoirs Online Hydraulic Modeling Results



Seattle Fault Seismic Event Transmission Pipeline Simulations

Case 2045 BWater from Tolt Filtration Plant cannot be conveyed west;
Eastside Supply Line is open; Tolt Eastside Pipes 7623, 7113, 7079, 7509 are closed;
Facility upgrades are the same as distribution system Case 3 (Volunteer and Roosevelt
Reservoirs are) online;
Water from Control Works (Cedar System) cannot be conveyed into the distibution

system.

Model Results

		Emitter			
Time	Total System	Flows	Supplied Demands	System Positive	Available System
(hrs)	Demand (gpm)	(gpm)	(gpm)	Pressure (%)	Storage (MG)
0	359,447	299,262	60,184	80%	352.9
3	324,619	268,614	56,005	77%	292.1
12	229,304	186,517	42,788	54%	146.1
22	81,487	52,044	29,443	25%	53.3
32	62,803	39,601	23,202	9%	15.2
48	24,771	17,638	7,133	6%	11.6

Model Regions Forced Out of Service During Simulation

Time	Region
9	S6
15	S1
20	S2
26	S8
32	S3
32	S4
33	T1

Model Simulation Notes

- 1. All wholesale customers assumed to start with 1.8 multiplier (max day demands)
- 2. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- 3. Total Model Demands with elevated wholesale customers is 91,957 gpm
- 4. Satisfied Demands assume junction pressure greater than 0 psi
- System Positive Pressure based on number of junctions above 0 psi out of the entire model

Model Results Figure Index

Fig. 13.1	Hr0 F	ig. 13.5	H r 8	Fig. 13.9	⊣r 16	Fig. 13.13	H r 2 4	Fig. 13.17	H r 40
Fig. 13.2	Hr2 F	ig. 13.6	Hr 10	Fig. 13.10	⊣r 18	Fig. 13.14	Hr 28	Fig. 13.18	H r 44
Fig. 13.3	Hr4 F	ig. 13.7	Hr 12	Fig. 13.11	⊣r 20	Fig. 13.15	Hr 32	Fig. 13.19	H r 48
Fig. 13.4	Hr6 F	ig. 13.8	Hr 14	Fig. 13.12	⊣r 22	Fig. 13.16	Hr 36	-	









































M7.0 Seattle Fault Zone Transmission Pipeline Year 2075 Improvement Case Hydraulic Modeling Results



Seattle Fault Seismic Event Transmission Pipeline Simulations

Case 2075 ATolt Filtration Plant supplies west up to Pipe 7031, not connected to
the rest of the system;
From the Control Works (Cedar System), there is only a single 60-inch diameter
pipeline that serves Seattle;
Eastside Supply Line, West Seattle Pipeline and Cedar River Pipeline #4 are online;
Facility upgrades are the same as the distribution system Case 2.

Model Results

		Emitter			
Time	Total System	Flows	Supplied Demands	System Positive	Available System
(hrs)	Demand (gpm)	(gpm)	(gpm)	Pressure (%)	Storage (MG)
0	395,094	307,309	87,785	85%	306.6
3	377,182	289,801	87,381	84%	254.2
12	333,482	249,800	83,682	73%	130.5
22	228,458	170,381	58,077	52%	63.5
32	204,855	146,999	57,856	52%	48.9
48	179,129	121,919	57,210	49%	33.2

Model Regions Forced Out of Service Durina Simulation

Service During Simula					
Time	Region				
12	S7				
21	S4				
21	S8				

Model Simulation Notes

- 1. All wholesale customers assumed to start with 1.8 multiplier (max day demands)
- 2. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- 3. Total Model Demands with elevated wholesale customers is 91,957 gpm
- 4. Satisfied Demands assume junction pressure greater than 0 psi
- System Positive Pressure based on number of junctions above 0 psi out of the entire model

Model Results Figure Index

Fig. 14.1	Hr O Fig.	14.5 Hr 8	Fig. 14.9	Hr 16	Fig. 14.13	H r 2 4	Fig. 14.17	Hr 40
Fig. 14.2	Hr 2 Fig.	14.6 Hr 10	Fig. 14.10	Hr 18	Fig. 14.14	Hr 28	Fig. 14.18	H r 44
Fig. 14.3	Hr4 Fig.	14.7 Hr 12	Fig. 14.11	Hr 20	Fig. 14.15	Hr 32	Fig. 14.19	H r 48
Fig. 14.4	Hr 6 Fig.	14.8 Hr 14	Fig. 14.12	Hr 22	Fig. 14.16	Hr 36		







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M7.0 Seattle Fault Zone Transmission Pipeline Year 2075 Improvement Case with Roosevelt and Volunteer Reservoirs Online Hydraulic Modeling Results



Seattle Fault Seismic Event Transmission Pipeline Simulations

Case 2075 BTolt Filtration Plant supplies west up to Pipe 7031, not connected to
the rest of the system;
From the Control Works (Cedar System), there is only a single 60-inch diameter
pipeline that serves Seattle;
Eastside Supply Line, West Seattle Pipeline, and Cedar River Pipeline #4 are online;
Facility upgrades are the same as the distribution system Case 4 (Volunteer and
Roosevelt Reservoirs are online).

Model Results

		Emitter			
Time	Total System	Flows	Supplied Demands	System Positive	Available System
(hrs)	Demand (gpm)	(gpm)	(gpm)	Pressure (%)	Storage (MG)
0	410,689	321,276	89,413	92%	360.1
3	377,468	288,653	88,815	89%	304.8
12	341,173	256,650	84,523	76%	169.6
22	269,239	206,456	62,782	69%	81.1
32	222,613	161,982	60,632	62%	50.1
48	179,247	122,256	56,991	48%	33.3

Model Regions Forced Out of Service During Simulation

Service D	uring Simula
Time	Region
12	S7
21	S4
21	S8

Model Simulation Notes

- 1. All wholesale customers assumed to have max day demands with 1.8 multiplier
- 2. Normal Systemwide Model Minimum Day Demand is 51,716 gpm
- 3. Total Model Demands with elevated wholesale customers is 91,957 gpm
- 4. Satisfied Demands assume junction pressure greater than 0 psi
- System Positive Pressure based on number of junctions above 0 psi out of the entire model

Model Results Figure Index

Fig. 15.1	Hr O	Fig. 15.5	H r 8	Fig. 15.9	H r 16	Fig. 15.13	Hr 24	Fig. 15.17	Hr 40
Fig. 15.2	H r 2	Fig. 15.6	Hr 10	Fig. 15.10	H r 18	Fig. 15.14	Hr 28	Fig. 15.18	H r 44
Fig. 15.3	H r 4	Fig. 15.7	Hr 12	Fig. 15.11	Hr 20	Fig. 15.15	Hr 32	Fig. 15.19	Hr 48
Fig. 15.4	Hr6	Fig. 15.8	Hr 14	Fig. 15.12	Hr 22	Fig. 15.16	Hr 36		









































APPENDIX C – REPRESENTATIVE WATER UTILITY PERFORMANCE GOALS

KEY TO THE TABLE

TARGET TIMEFRAME FOR RECOVERY:

Desired time to restore component to 80–90% operational Desired time to restore component to 50–60% operational Desired time to restore component to 20–30% operational Current State (90% operational)



TARGET STATES OF RECOVERY: WATER & WASTEWATER SECTOR (COAST)											
	Event occur s	0–24 hours	1–3 days	3–7 days	1–2 weeks	2 weeks -1 month	1–3 month s	3–6 month s	6 month s–1 year	1–3 years	3+ years
Domestic Water Supply											
Potable water available at supply source (WTP, wells, impoundment)				R		Y		G		x	
Main transmission facilities, pipes, pump stations, and reservoirs (backbone) operational			R	Y	G					x	
Water supply to critical facilities available				R		Y		G		x	
Water for fire suppression—at key supply points			R		Y			G		x	
Water for fire suppression—at fire hydrants						8	Y	G		x	
Water available at community distribution centers/points				R	Y	G	x		2	-	
Distribution system operational					R		Y	G			x

Table C-1. Oregon Resilience Plan (2013) Water System Post-Earthquake Recovery Targets for Coastal Communities (Stronger Ground Shaking than Willamette Valley)

KEY TO THE TABLE

TARGET TIMEFRAME FOR RECOVERY:

Desired time to restore component to 80–90% operational Desired time to restore component to 50–60% operational

Desired time to restore component to 20-30% operational

Current state (90% operational)

G
Y
R
×

TARGET STATES OF RECOVERY: WATER & WASTEWATER SECTOR (VALLEY)											
	Event occurs	0–24 hours	1–3 days	3–7 days	1–2 weeks	2 weeks– 1 month	1–3 months	3–6 months	6 months –1 year	1–3 years	3 + years
Domestic Water Supply											
Potable water available at supply source (WTP, wells, impoundment)		R	Y		G			x			
Main transmission facilities, pipes, pump stations, and reservoirs (backbone) operational		G					x				
Water supply to critical facilities available		Y	G				x				
Water for fire suppression—at key supply points		G		x							
Water for fire suppression—at fire hydrants				R	Y	G			x		
Water available at community distribution centers/points			Y	G	x						
Distribution system operational			R	Y	G				x		

Table C-2. Oregon Resilience Plan (2013) Water System Post-Earthquake Recovery Targets for Willamette Valley Communities (Lower Ground Shaking than Oregon Coast)

KEY TO THE TABLE

TARGET TIMEFRAME FOR RECOVERY:

TARGET TIMEFRAME FOR RECOVERY:				
Operational (time it ought to take to restore component to 80–90% operational):				
TIME NEEDED FOR RECOVERY TO 80-90% OPERATIONAL GIVEN CURRENT CONDITIONS:	×			
TIME NEEDED FOR RECOVERY TO 80-90% OPERATIONAL IN LIQUEFACTION ZONES GIVEN CURRENT CONDITIONS:				
TIME NEEDED FOR RECOVERY TO 80-90% OPERATIONAL IN NON-LIQUEFACTION ZONES GIVEN CURRENT CONDITIONS:	NL			

TARGET STATES OF RECOVERY: WASHINGTON'S UTILITIES SECTOR									
	Event occurs	0–24 hours	1–3 days	3–7 days	1 week- 1 month	1–3 months	3 months- 1 year	1–3 years	3+ years
Domestic water supply	T								
Supply & transmission pipes				NL			L		
Distribution pipes					NL		L		
Wastewater systems									
Treatment facilities						NL	L		
Sewer pipes]	NL		L	
Flood control	ĺ							ĺ	
Dams						×			
Levees								×	
Electricity									
Transmission								×	
Distribution, 60% restored					×				
Distribution, 70% restored						×			
Distribution, >70% restored							×		
Natural Gas									
Transmission			NL		L				
Distribution, 40% restored					×				
Distribution, 90% restored						×			
Petroleum									
Refineries & transmission								×	
Distribution						×			
Information and communication technology						×			

Table C-3. Resilient Washington State (2012) Lifeline Post-Earthquake Recovery Targets

Service Category		Probable Earthquake
General	1	Minimal secondary damage and risk to the public
	2	Limit extensive damage to system facilities
	3	All water introduced into the distribution system minimally disinfected
	4	All water introduced into the distribution system fully treated
Fire Service	5	Sufficient portable pumps and hose to provide limited fire service in all areas
	6	All areas have minimal fire service (one reliable pumping plant and reservoir)
	7	High risk areas have improved fire service (all facilities reliable, minimum fire reserves)
	8	Normal service to all hydrants within 20 days
Hospitals and Disaster Centers	9	Minimum service to affected area within 1 day (water available via distribution system near each facility)
	10	Impaired service to affected area within 3 days (water available via distribution system to each facility, possibly at reduced pressures)
Domestic Users	11	Potable water via distribution system or truck within 1 day
	12	Impaired service to affected area within 3 days (water available via distribution system to each domestic user, possibly at reduced pressures)
Commercial, Industrial and Other Users	13	Impaired service to affected area within 3 days (water available via distribution system to each commercial or industrial user, possibly at reduced pressures)

Table C-4. East Bay Municipal Utility District (EBMUD) Post-Earthquake Performance Goals for A "Probable" Earthquake (e.g., M6 Hayward Fault Event within the EBMUD Service Area or Larger Event Outside the EBMUD Service Area) (Eidinger and Davis 2012)

Service Category		Maximum Earthquake
General	1	Minimal secondary damage and risk to the public
	2	Limit extensive damage to system facilities
	3	All water introduced into the distribution system minimally disinfected
	4	All water introduced into the distribution system fully treated
Fire Service	5	Sufficient portable pumps and hose to provide limited fire service in all areas
	6	All areas have minimal fire service (one reliable pumping plant and reservoir)
	7	High risk areas have improved fire service (all facilities reliable, minimum fire reserves)
	8	Normal service to all hydrants within 100 days
Hospitals and Disaster	9	Minimum service via distribution system or truck within 3 days
Centers	10	Minimum service within 10 days (water available via distribution system near each facility)
	11	Impaired service within 30 days (water available via distribution system to each facility, possibly at reduced pressures)
Domestic Users	12	Potable water at central locations for pickup within 3 days
	13	Minimum service to 70% of customers within 10 days
Commercial, Industrial and	14	Potable water at central locations for pickup within 1 week
Other Users	15	Minimum service to 70% of customers within 10 days
	16	Impaired service to 90% of customers within 30 days (water available via distribution system to 90% of commercial or industrial users, possibly at reduced pressures)

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Table C-5. East Bay Municipal Utility District (EBMUD) Post-Earthquake Performance Goals for A "Maximum" Earthquake (e.g., A Hayward Fault Event Where the Fault Ruptures Along The Entire Length Within the EBMUD Service Area) (Eidinger and Davis 2012)
Service Category		Probable Earthquake	
General	1	Minimal secondary damage and risk to the public	
	2	Limit extensive damage to system facilities	
	3	All water introduced into the distribution system minimally disinfected	
Fire Service	4	Provide 100% of average winter level flows to customer meters within 4 hours after earthquake. (Tentative goal for large customers)	
	5	Provide 100% of average winter level flows to all customer meters within 3 days after earthquake. (Tentative goal for large customers)	
Domestic Water Service	6	6 Potable water via truck or accessible locations within 1 day to meet minimum consumption needs (1 gallon per person per day)	
	7	Impaired service within 3 days	
	8	Normal service within 20 days	
Raw Water Service	9	Impaired service within 3 days	
	10	Normal service within 20 days	

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Minimally Disinfected	Chlorination or better.
Impaired Service	Provide water (adequate to meet winter time demands), possibly at lower pressure than normal.
Normal service co	Provide water at the same level of reliability as under "normal" pre-earthquake nditions.

Figure C-6. Humboldt Bay Municipal Water District Post-Earthquake Performance Goals for a Probable Earthquake (Eidinger and Davis 2012)

Service Category		Maximum Earthquake	
General	1	Minimal secondary damage and risk to the public	
	2	Limit extensive damage to system facilities	
	3	All water introduced into the distribution system minimally disinfected	
Fire Service	4	Provide 50% of average winter level flows to customer meters within 4	
		hours after earthquake. (Tentative goal for large customers)	
	5	Provide 100% of average winter level flows to all customer meters	
		within 3 days after earthquake. (Tentative goal for large customers)	
Domestic Water Service	6	Potable water via truck or accessible locations within 1 day to meet	
		minimum consumption needs (1 gallon per person per day)	
	7	Impaired service within 7 days	
	8	Normal service within 60 days	
Raw Water Service	9	Impaired service within 7 days	
	10	Normal service within 60 days	

Minimally Disinfected	Chlorination or better.
Impaired Service	Provide water (adequate to meet winter time demands), possibly at lower pressure than normal.
Normal service co	Provide water at the same level of reliability as under "normal" pre-earthquake nditions.

Figure C-7. Humboldt Bay Municipal Water District Post-Earthquake Performance Goals for a Maximum Earthquake (Eidinger and Davis 2012)

	Hazard Return	
Level	Period Criteria	Target Water System Performance
1	100 years	Limited damage to water system, no casualties, few to no water service losses. All customer services operational within about 3 days.
2	500 years	Life safety and property protection. All customer services
		operational within about 20 days, except water quantity; rationing
		may extend up to 30 days.
3	2500 years ¹	Life safety and property protection. All customer services
		operational within about 30 days, except water quantity; rationing
		may extend up to 60 days.
4	> 2500 years	Life safety and property protection. All customer services
	up to about	operational within about 45 days, except water quantity; rationing
	10,000 years	may extend up to 12 months.

1 – Highly active faults such as the San Andreas Fault have great earthquakes of $M_w > 7.8$ within these return periods, for which the performance criteria are proposed to meet Level 4.

Table C-8. Los Angeles Department of Water and Power Preliminary/Draft Post-Earthquake Performance Criteria (Davis 2017)

APPENDIX D – DRAFT SPU SEISMIC DESIGN STANDARDS FOR NEW PIPE

Scope

This standard applies to new watermain construction, including new pipelines that are replacing existing pipelines. Existing watermains need not adhere to these standards unless they are rehabilitated or replaced.

Adoption and Revisions/Updates

This draft standard will form the framework for SPU's seismic design standards for new watermains. Before these standards can be officially adopted by SPU, they will be reviewed by SPU design engineers and operations staff. The standards will be periodically updated to reflect the American Society of Civil Engineers (ASCE) Manual of Practice (MOP) on seismic design guidelines for water and wastewater pipelines that is currently being developed, seismic hazard mapping changes that occur in the SPU transmission and distribution area, and new earthquake resistant pipe systems that are being developed.

Definitions

<u>Primary Backbone Pipelines</u>–Transmission pipelines that convey water from the Tolt Reservoir or Lake Youngs Treatment Plant to the terminal reservoirs. Primary Backbone Pipelines are identified in Figures 1 and 2.

Secondary Backbone Pipelines-Transmission

pipelines that convey water from the terminal reservoirs to distribution reservoirs or large service areas. Because Lake Youngs can supply the Cedar system for four weeks, the transmission pipelines from the Landsburg Diversion to Lake Young are defined as secondary backbone pipelines. Secondary Backbone Pipelines are identified in Figures 1 and 2.

<u>Hospital/Critical Facility Watermains</u>–Watermains that are needed to supply hospitals or other critical facilities that must remain operational after an earthquake. Hospital/Critical Facility Watermains are identified in Figure 2.

<u>Fire-fighting Mains</u>—Mains needed to supply water to within 2,500 feet of anywhere in the City of Seattle. Fire-fighting mains are identified in Figure 2.

<u>Ordinary Mains</u>–All watermains that are not classified as backbone, hospital/critical facility or firefighting mains.

<u>Permanent Ground Displacement (PGD)-Susceptible Area</u> – Those areas (see Figures 1 and 2 that are

1. Identified by Palmer et al. (2004) as having a high- or moderate-to-high liquefaction susceptibility or peat area, or

- 2. Defined by the Seattle Department of Construction and Inspection to be in a Known or Potential Slide Area, or
- 3. Defined as a King County Landslide Hazard Area, or
- 4. Defined as a Washington Division of Geology and Earth Resources Landslide Area.

If a geotechnical investigation shows that PGD is possible along the alignment, even though the alignment is not within one of the PGD-susceptible areas identified in Figures 1 or 2, then that pipeline shall be considered to be in a PGD-susceptible area. Alternatively, if a geotechnical investigation shows that the pipeline alignment is not susceptible to PGD, even though the alignment lies within a PGD-susceptible area identified on Figures 1 or 2, the pipeline may be designed as if it does not lie in a PGD-susceptible area.

<u>Seattle Fault Zone</u>–That area defined by Pratt et al. (2015) as adopted by Lettis Consultants International, Inc. (2016) as being in Zone A or Zone B as depicted in Figure 1.

<u>SPU Intense Ground Shaking Region</u>—The area within the SPU transmission and distribution region where the 0.02 probability of exceedance in 50-year ground motions are greater than or equal to 0.6g (see Figure 2).

SPU Watermain Seismic Design and Construction Requirements

The level of analysis and performance required for watermain design and construction shall be in accordance with the watermain criticality and earthquake hazard exposure as defined in Table 1. Primary and secondary backbone pipelines, hospital/critical facility and firefighting mains are identified in Figures 1 and 2. For any pipeline, if a site-specific analysis shows a lesser level of design than that stipulated by Table 1 is adequate, then that pipeline need only be designed in accordance with the design indicated by the site-specific analysis.

Table 1. Minimum	Watermain	Design ar	d Constru	ction Analy	sis and	Performance
<u>Requirements</u>						

Watermain Class/Criticality	PGD Area	Seattle Fault Zone or SPU Intense Ground Shaking Region	All Other Areas
Ordinary	Performance Specification 1	Performance Specification 2	No seismic requirements
Hospital/Critical Facility and Fire Fighting Mains	Performance Specification 1	Performance Specification 1	Performance Specification 1
Secondary Backbone	Site-specific analysis	Site-specific analysis	Performance Specification 1
Primary Backbone	Site-specific analysis	Site-specific analysis	Site-specific analysis

Performance Specification 1 Requirements

To meet the requirements for Performance Specification 1, pipelines must meet the following ductility and strength requirements:

1) Segmented Ductile Iron Pipelines

Axial Elongation: 1% Minimum Axial Elongation or Shortening.

Axial Pullout Strength: 17,130 pounds per inch diameter

<u>Deflection:</u> 5 degrees of deflection must be provided at each joint per 20-foot segment. Prorate for shorter or longer segment lengths. Maximum segment length is 30 feet.

Segmented pipeline systems that meet the Performance Specification 1 requirements include, but are not limited to

- Kubota Genex Earthquake Resistant Ductile Iron Pipe
- American Pipe Earthquake Joint Pipe

2) Continuous Pipelines

a) Welded Steel Pipelines with Butt-Welded Joints – Meet the requirements of AWWA C200 and

$$\frac{D^2}{12t} \le 537$$

Where D = the pipe diameter in inches

t = the pipe wall thickness in inches

b) HDPE Pipelines – Meet the requirements of AWWA C906 and ASTM F2620.

<u>Pipeline Backfill/Bedding:</u> Pipe backfill and bedding shall be as specified in Standard Plan 350 of Seattle Standard Plans for Municipal Construction. The use of Control Density Fill or other backfill/bedding that could restrict pipe movement is not permitted.

Performance Specification 2 Requirements

The following pipelines are permitted in Performance Specification 2 areas:

- Restrained joint ductile iron pipe that conforms to the City of Seattle Standard Specifications and Plans. Additionally, for restrained joint ductile iron pipe that is being restrained only to address seismic concerns, Series 1100 MegaLug restrained joints are acceptable.
- 2) Welded steel pipe joint with either lap or butt welds
- 3) HDPE pipe that meets the requirements of AWWA C906 and ASTM F2620

4) Restrained joint, molecularly oriented polyvinyl chloride pipe (PVC O) that meets the requirements of AWWA C909.

Site-specific analysis:

The site-specific analysis shall meet the following minimum requirements

- 1. Geotechnical hazards shall be identified and evaluated along the pipeline alignment.
 - a. Geotechnical hazards shall be consistent with those hazards that would occur from 0.02 probability of exceedance in 50 years (2475 average return interval) ground motions.
 - b. Geotechnical hazards shall include transient seismic wave propagation/ground shaking hazards and PGD hazards.
- 2. The pipeline shall be designed and constructed to resist and accommodate the forces and ground motions/displacements along the alignment determined in Step 1. The following criteria must be met:
 - a. The pipeline shall remain operable during and after the seismic event.
 - b. Inelastic behavior, possibly requiring eventual repair or replacement, is allowable providing the pipeline can remain operable until the post-earthquake emergency conditions have passed.
 - c. The larger of either the mean or medium values of the estimated geotechnical hazards (e.g., permanent ground displacement, peak ground velocity, etc.) shall be used in the analysis.
 - d. Pipe material and system properties will be as specified by the appropriate ASTM standard with a factor of safety equal to 1.0.

<u>No seismic requirements:</u> New pipelines need only meet SPU non-seismic specific requirements.

Hydrants

For hydrant runs in PGD areas, accommodation shall be made within 10 feet of the hydrant connected to allow for a minimum of five degrees of rotation and two inches of expansion or contraction between the main and hydrant piping. Hydrant connection piping shall be restrained joint ductile iron, welded joint welded steel or HDPE with thermally fused joints.

Services

Services shall be protected by a fabricated steel sleeve that is connected to a semirigid sleeve as shown in Figure 3. The sleeves shall allow the service to move 2-inches of vertical or axial direction pipe movement. If a valve box is needed, a vertical semirigid sleeve is also needed



Figure 1. SPU Water Systems Hazards Map



Figure 2. Direct Service Area Seismic Hazards and Critical Pipelines



Figure 3. Service Connection

Appendix D References

Lettis Consultants International, 2016, *Final Desktop review and Summary of the Seattle and South Whidbey Island Fault Zones for Seattle Public Utilities.*

Palmer, Stephen P., et. Al., 2004, *Liquefaction Susceptibility and Site Class Maps of Washington State, By County*, Washington Division of Geology and Earth Resources, Open File Report 2004-20.

Pratt, T.L., Troost, K.G., Odum, J.K., and Stephenson, W.J., 2015, "Kinematics of Shallow Backthrusts in the Seattle Fault Zone," *Washington State: Geosphere* 11, No. 6, doi.10.1130/GES01179.1.